



UNIVERSITÀ DI PISA



Gruppo Ricerca Nucleare S. Piero a Grado

Recent Applications of RELAP5-3D at GRNSPG

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CONTENTS

- CNA2 : FSAR activities
- Standard Consolidated Reference Experimental Database
- MASLWR benchmark
- OECD benchmarks
- CHF calculation in low mass flux condition
- Turbulence effects in Relap5-3D



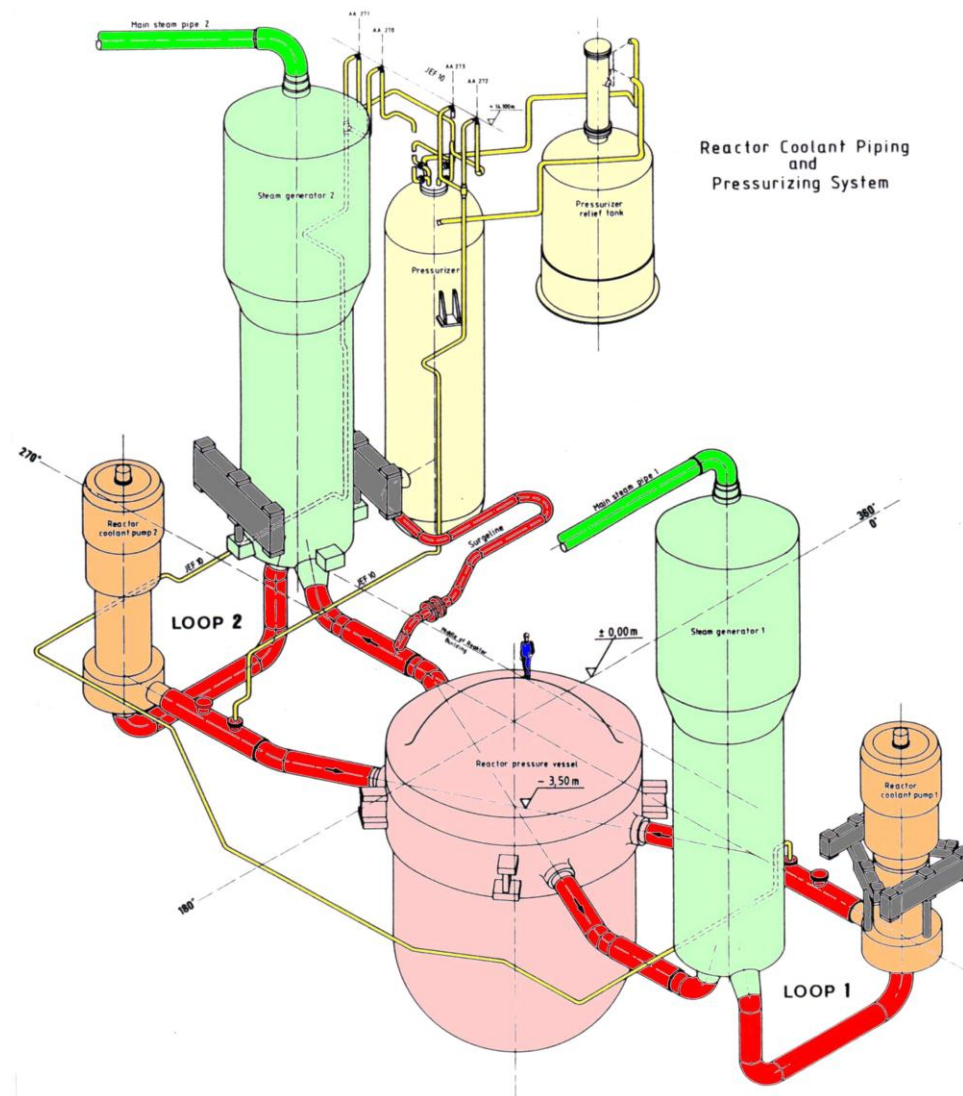
The Atucha-2 NPP

- ❑ **CNA2 – Chapter 15 FSAR – one of the main projects of GRNSPG 2007-2012**
 - BEPU approach
- ❑ **Relap5-3D main tool for analysis**
- ❑ **Applications (main)**
 - Three different nodalizations for RCS
 - 3D Neutron Kinetic
 - Coupling to code modeling I&C
- ❑ **LOCA recalculation and qualification activities in 2011-2012**



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2 LOOPS

1 MCP, 1 UT SG each

1 PRZ

2160 MWth

1958 + 203 (nom. mod. T), or
2001 + 160 (max mod T)

+

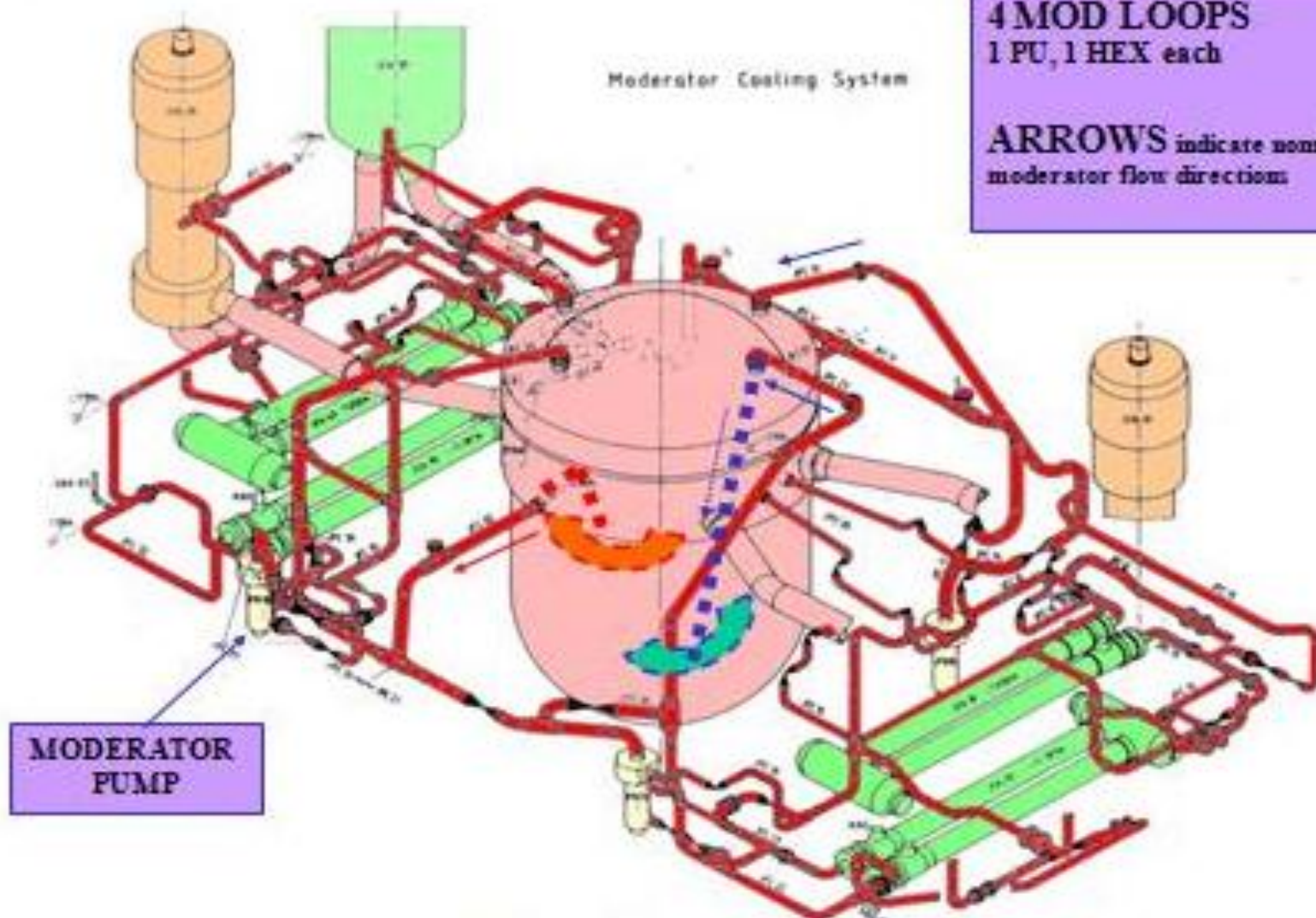
14 from MCP

451 separated FC



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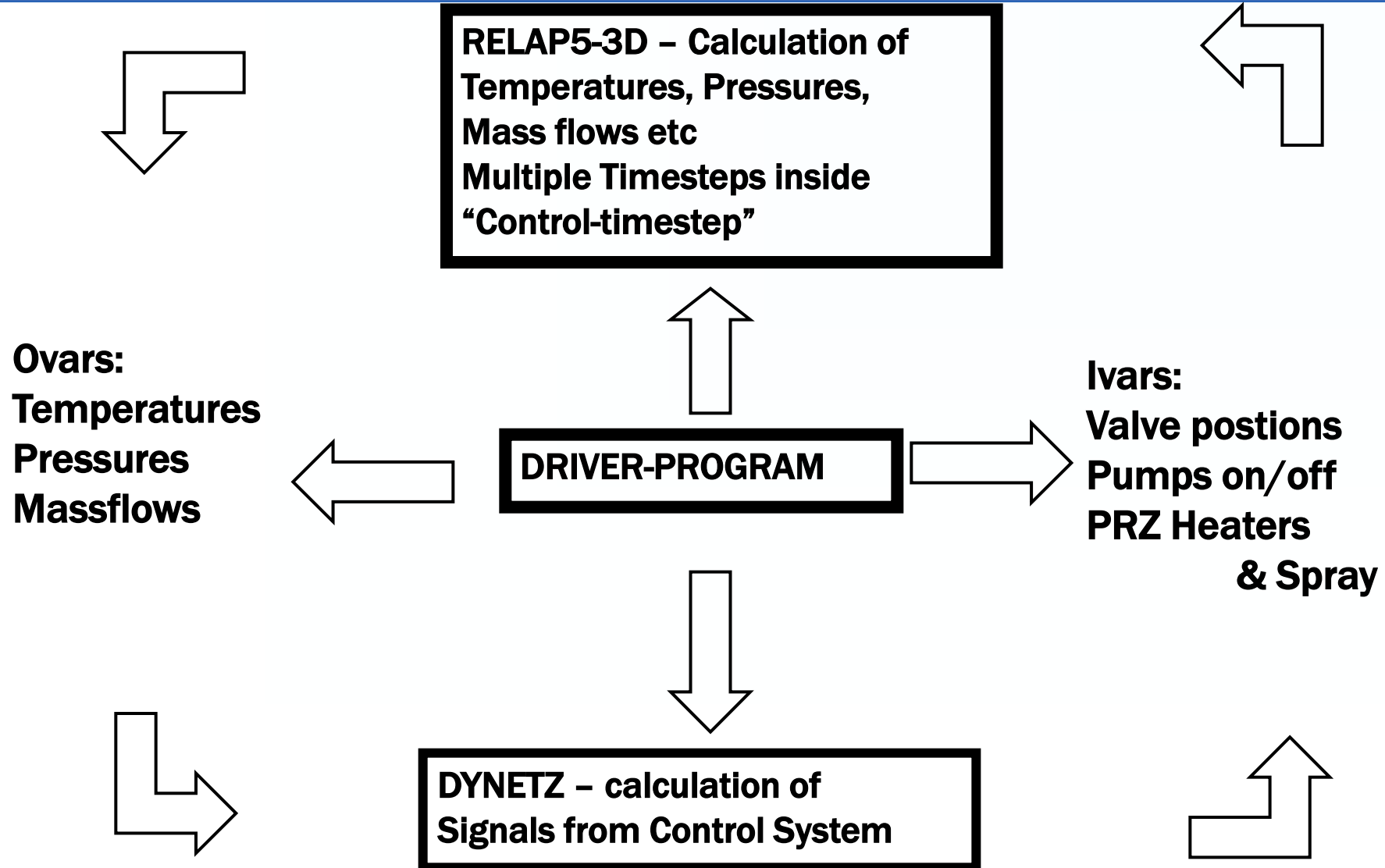
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| No | Transient | Section FSAR | Adopted Evaluation Model | Class of Accident |
|---|---|--------------|--------------------------|-------------------|
| Decrease in Reactor Coolant System Inventory (part 2 of 2) | | 15.6 | | |
| | Spectrum of LOCA | 15.6.5 | - | - |
| | Primary Coolant System LOCA | 15.6.5.1 | - | - |
| | Small Break LOCA | 15.6.5.1.1 | - | - |
| 50 | 30 cm ² LOCA cold | 15.6.5.1.1.1 | CSA | DBA |
| 51 | 100 cm ² LOCA cold | 15.6.5.1.1.2 | CSA | DBA |
| 52 | Break of the Refueling Nipple | 15.6.5.1.1.3 | CSA | DBA |
| | Intermediate Break LOCA | 15.6.5.1.2 | - | - |
| 53 | 200 cm ² LOCA cold | 15.6.5.1.2.1 | CSA/CBA | DBA |
| 54 | LOCA in PRZ Surge-Line | 15.6.5.1.2.2 | CSA | DBA |
| 55 | 0.1A LOCA cold <input type="checkbox"/> | 15.6.5.1.2.3 | CSA/RCA/CBA | DBA |
| 56 | 0.1A LOCA cold with Sump Swell Operation <input type="checkbox"/> | 15.6.5.1.2.4 | QA | DBA |
| | Large Break LOCA | 15.6.5.1.3 | - | - |
| 57 | 2A LOCA cold (<i>DEGB. Different Break Sizes and Positions are investigated</i>) <input type="checkbox"/> | 15.6.5.1.3.1 | CSA/RCA/CBA | SBDDBA |
| 58 | 2A LOCA hot <input type="checkbox"/> | 15.6.5.1.3.2 | CSA/CBA | SBDDBA |
| | Moderator LOCA | 15.6.5.2 | - | - |
| 59 | 50 cm ² Small Leak in Moderator Suction Line | 15.6.5.2.1 | CSA | DBA |

83 NPP Scenarios



The Atucha-2 NPP





The Atucha-2 NPP

□ 2011-2012 Activities

- LOCA recalculation
- Use of internal coupling solution for I&C (developed by NA-SA)
- Qualification
- Consolidate data bases (QA related)
- Visualization



The Atucha-2 NPP

- Facility and experiments used in qualification activity related to CNA2 project:

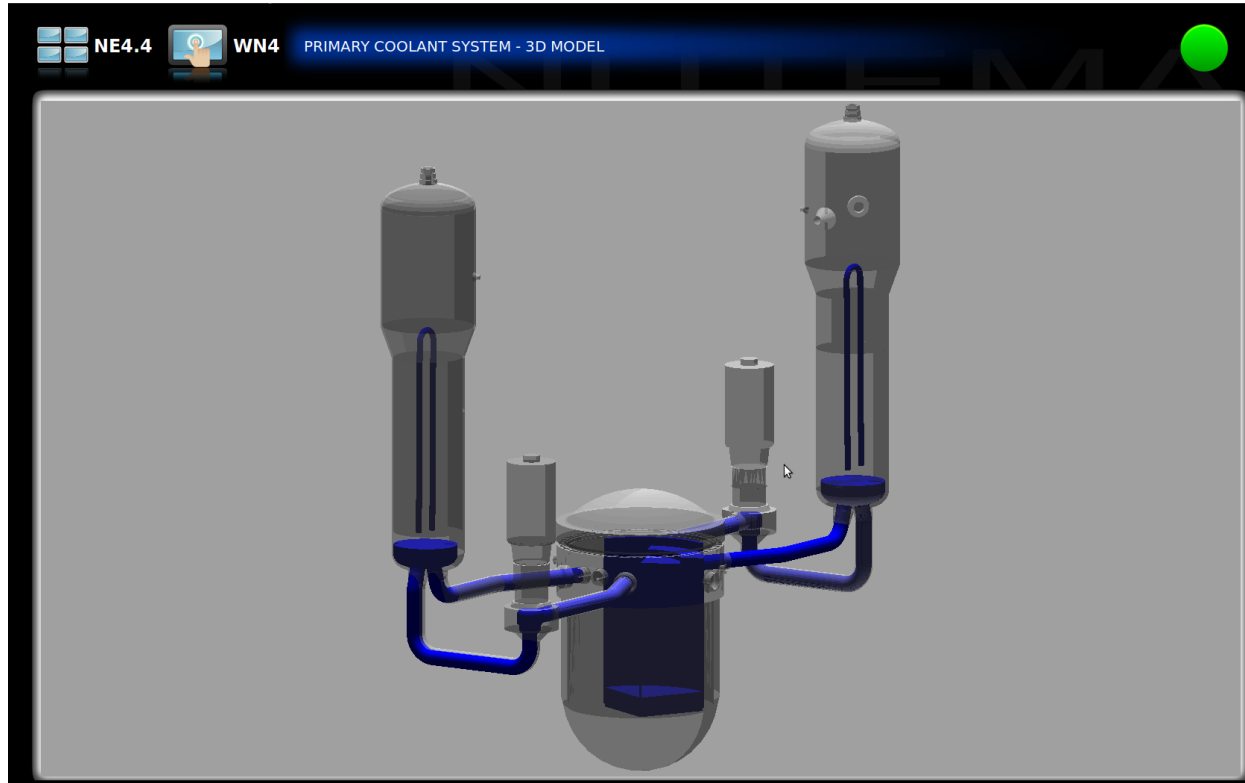
| Experimental Test | Transient Type |
|-------------------|---|
| PSB-VVER T#3 | Stuck open PRZ safety valve |
| PSB-VVER T#5 | Main Steam Line Break + SGTR |
| LOBI A2-81 | 100 cm ² CL LOCA (0.7%) |
| SPES SP-SB-04 | 200 cm ² CL LOCA (4.2%) |
| LOBI A1-83 | 0.1 A CL LOCA |
| LOBI BT-15 | Loss of one MFW pump without starting of the reserve pump |
| LOFT L2-5 | 2A CL LOCA |
| LOBI A1-06 | |
| UPTF 05 | |

Correspondence with FSAR scenarios



The Atucha-2 NPP

- In the framework of NUTEMA project one of the most interesting features related to Relap5 is the 3D visualizer.
 - read 3ds data file (Pro Engineer and other)
 - Relap5-3D results can be mapped onto the CAD model
 - Fast and fluently displayed with OpenGL libraries



Void distribution
in PS during the
early phase of a
SBLOCA



SCRED: Standard Consolidated Reference Experimental Database

- ❑ Availability of Experimental Data might not be enough:
 - Information spread on several reports
 - Different quality level and format of the documentation
 - Need to explain and clarify the information
 - Contradictions exist
- ❑ Preserving the Experimental Data shall be a MUST
- ❑ Qualified experimental database is envisaged by IAEA (SRS 23)
- ❑ Need for a Standard for fully exploit the experimental data and generate a Consolidated Reference Experimental Database (SCRED)
- ❑ Use of SCRED for:
 - Code Assessment
 - Uncertainty Evaluation



SCRED: Development of the Methodology

- ❑ Development of a methodology for collecting, organizing, using and preserving an exhaustive set of geometrical data and experimental results
 - Exhaustive consolidated information,
 - Traceability
 - Use of a Standard Format
 - Documentation of the decisions taken in case of lack of data or in presence of contradictory information
- ❑ Development of a **Reference Data Set (RDS)** document for developing input nodalization
- ❑ Setting up standard procedures for using the collected data and qualify the code calculations (**Qualification Report, QR**)
- ❑ Development of a standard report (**Engineering Handbook, EH**) containing a full description of how the database has been converted into an input data deck for a specific computer code (support to verification)



SCRED main steps: RDS-Facility

Structure and sample, RDS-Facility

The **RDS-Facility** is related with the design in a “reference status” of a facility and consists of the following standard sections:

- Layout of the facility
- Collection of geometrical data (length, volumes, areas, elevations) for each subsystem and component of the facility
- Collection of specific data for complex component (pumps, valves, heaters, etc...)
- Identification of geometrical discontinuities and evaluation of pressure loss coefficients (normal operation)
- Material properties
- Measurement system
- Nominal heat losses
- Nuclear data (if available)

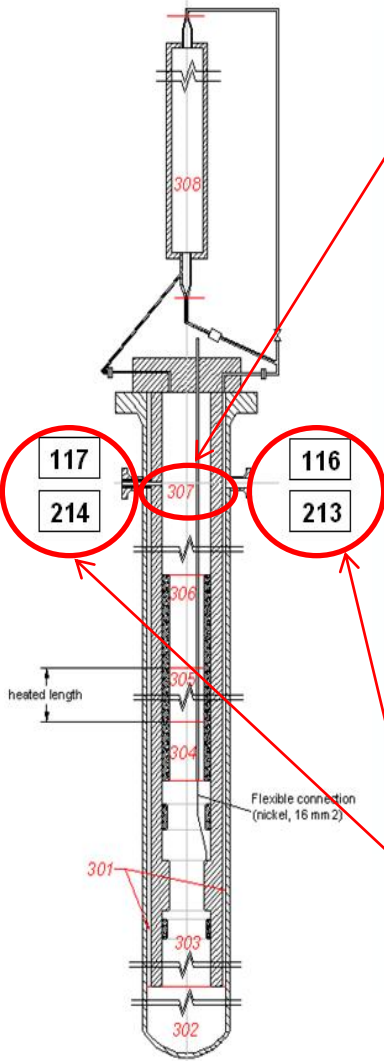
“**Reference status**” corresponds to a geometrical and hardware configuration of the facility at a certain time



SCRED main steps: RDS-Facility

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Structure and Sample, RDS-Facility



- **Module number**
- **Module location**
- **Module description**
- **Geometrical description**
- **Lengths**
- **Areas**
- **Volumes**
- **Pressure losses**
- **Connection to other modules**

| Pressure vessel | | | | |
|------------------------------|--|---------------------------|-------------------------|----------|
| Module number | 307 | | | |
| Description | Upper plenum part 2 | | Vertical parallelepiped | |
| Parameters | Evaluation | Value | Remarks | |
| Outer rod bundle diameter | $D_{\text{bundle}}=10.75 \text{ mm}$ | $1.075 \cdot 10^{-2}$ | m | Draw. 13 |
| Barrel inside diameter | $D_{\text{barrel}}=198 \text{ mm}$ | $1.98 \cdot 10^{-1}$ | m | |
| Barrel outside pipe diameter | $D_{\text{out}}=288 \text{ mm}$ | $2.88 \cdot 10^{-1}$ | m | Draw. 13 |
| Number of rod bundle | 64 | | | Draw. 13 |
| Length | $L=2015+328=2343 \text{ mm}$ | 2.343 | m | Draw. 13 |
| Elevation change | 2015 mm | 2.015 | m | |
| Flow area | $S=S1-S2$ $S1=\pi \cdot D_{\text{barrel}}^2/4=\pi \cdot 198^2/4=30790.7 \text{ mm}^2$ $S2=64 \cdot \pi \cdot D_{\text{bundle}}^2/4=64 \cdot \pi \cdot 10.75^2=5808.8 \text{ mm}^2$ | | m^2 | Draw. 13 |
| Inside surface area | $S=24981.9 \text{ mm}^2$ Heat exchange with downcomer $S_{\text{cylinder}} = 2 \pi \cdot R \cdot H$ $SA=\pi \cdot D_{\text{barrel}} \cdot L=\pi \cdot 198 \cdot 2343=1457428 \text{ mm}^2$ | $2.4982 \cdot 10^{-2}$ | m^2 | Draw. 13 |
| Outside surface area | Outer surface of barrel (part of module 301) $S_{\text{cylinder}} = 2 \pi \cdot R \cdot H$ $SA=\pi \cdot D_{\text{out}} \cdot L=\pi \cdot 288 \cdot 2343=2119896 \text{ mm}^2$ | | m^2 | |
| Volume | $24981.9 \cdot 2343=58532592 \text{ mm}^3$ | $5.8532592 \cdot 10^{-2}$ | m^3 | |
| Pressure loss coefficient | Expansion 307→308 $k_{\text{turn}}=0.5$ $k_{\text{rev}}=1$ | | | Tab. 4.2 |



SCRED main steps: RDS-Test

Structure and Sample, RDS-Test

Standard structure of the RDS-Test:

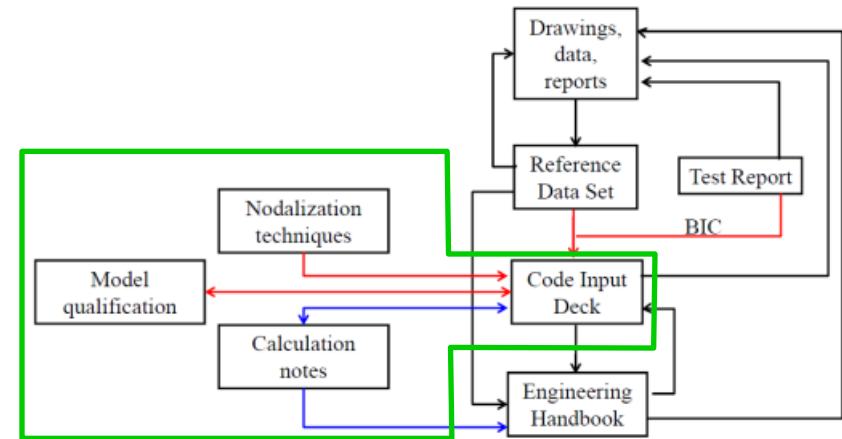
- Test objective
- Facility description
 - Test configuration
 - Difference between facility “reference status” and test configuration
- Test description
 - Initial condition
 - Boundary condition
- Thermal-hydraulic system behaviour
 - Main events and major phenomena
 - Thermal-hydraulic parameter trends (more than 40 time trends)



SCRED main steps: Input Files and Qualification Reports (QR)

Purpose

- ❑ Nodalization preparation: main choices of the model characteristics and preliminary code resources distribution (**data from RDS**)
- ❑ Nodalization schematization according to the **pre-set nodalization strategies**
- ❑ Writing input following a **pre-set structure**
- ❑ The **Qualification Report (QR)** collects the results of the qualification procedures of the code input and it is reviewed by the higher level analyst in the group

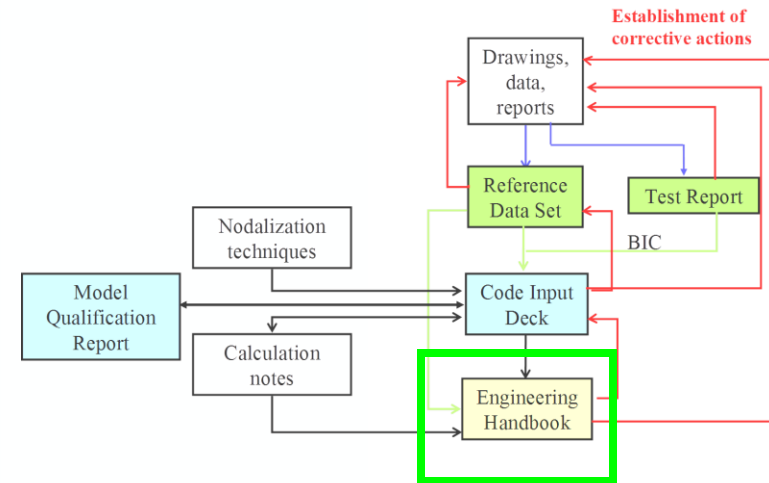




SCRED main steps: ENGINEERING HANDBOOK (EH)

Purpose

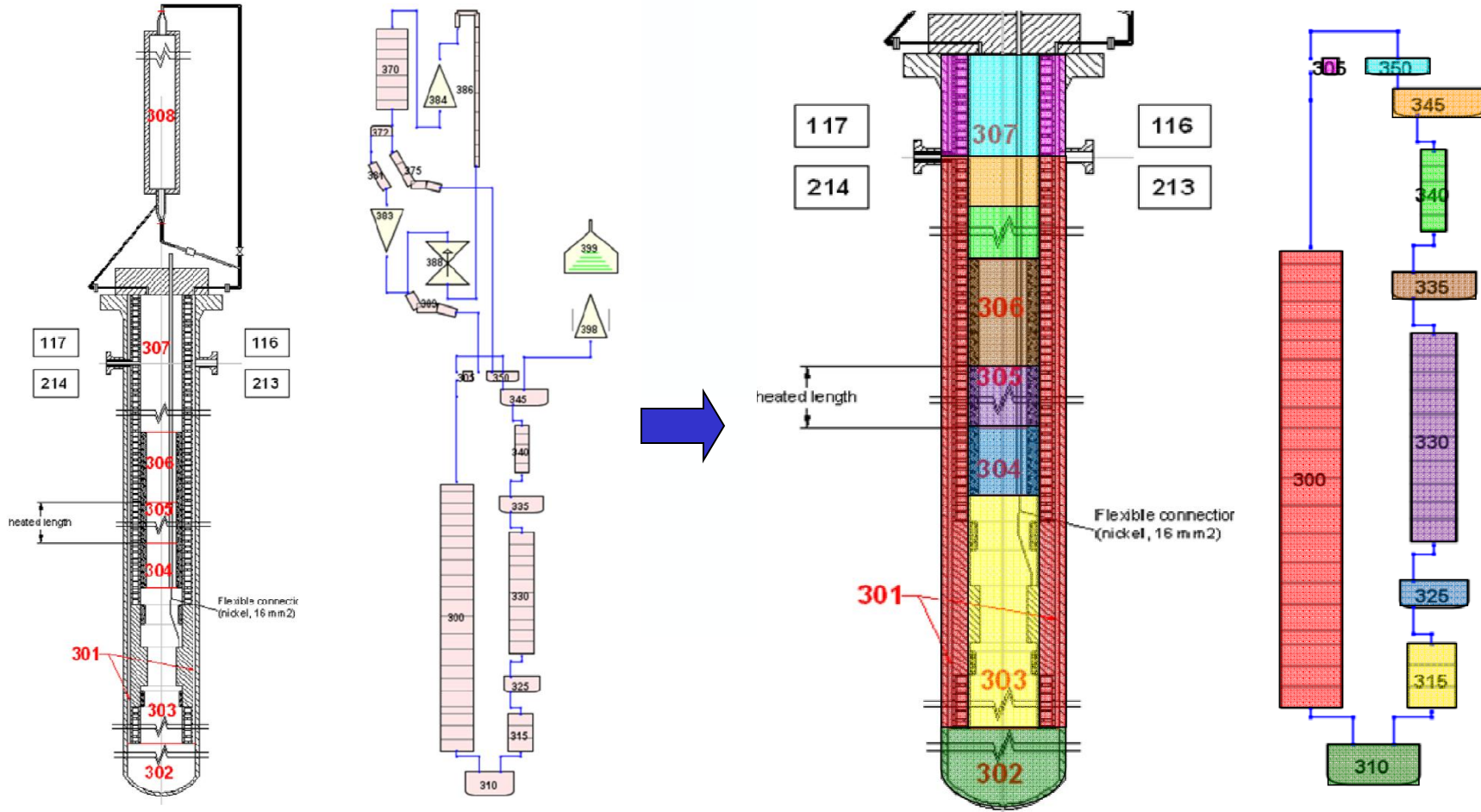
- EH contains the **technical rationale** for the **input**, provides the **engineering justifications** of the adopted **assumptions** and allows the **verification of the model's input file**
 - **Methods and assumptions used to convert the RDS-Facility and RDS-Test information into the code input data**
 - **Nodalization schemes of the components**
 - **The calculation notes (traceability of the information)**
 - **Adequate description and explanation of adopted modeling assumptions**





Structure and Sample, EH

□ Cross links between (RDS) Drawings and Nodalizations





SCRED achievements

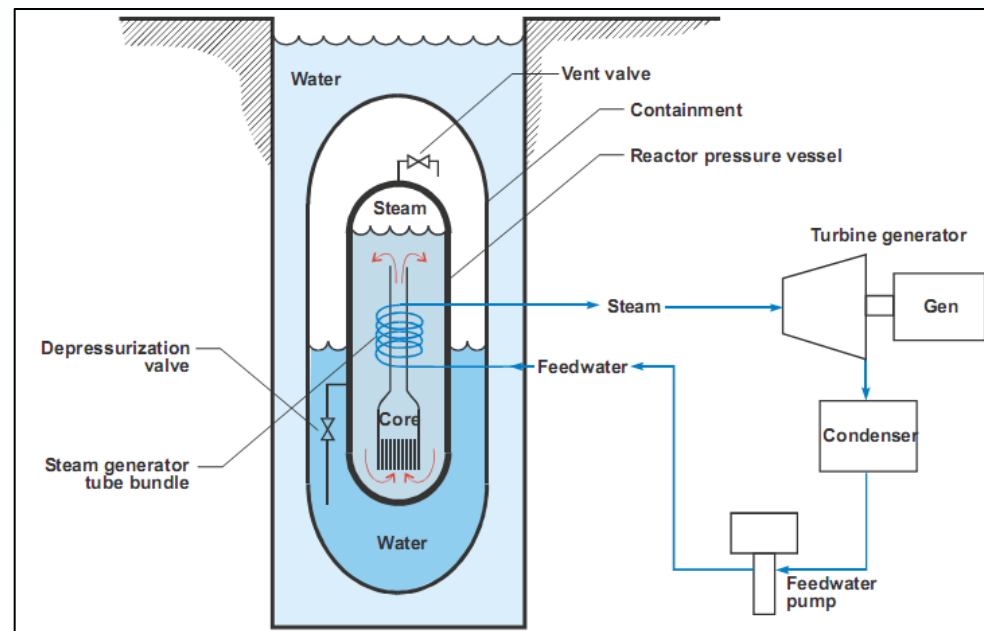
- ❑ A methodology to develop a Standard Consolidated Reference Experimental Database (SCRED) has been set-up
- ❑ Recommendations from IAEA guidelines have been considered
- ❑ The methodology ensures the fulfillment of QA through:
 - The application of a standard format
 - Strict observance of each step of the methodology
 - The development of RDS to consolidate in a standard way the experimental information
 - The application of a rigorous qualification process discussed in the QR
 - The verification of each value of the input file by the EH
- ❑ SCRED allows for an easier transfer in time and to different group of the experimental information and acquainted knowledge
- ❑ SCRED can be used for code assessment and uncertainty quantification



BENCHMARKING

- ❑ The **Multi-Application Small Light Water Reactor (MASLWR)** project was conducted under the auspices of the Nuclear Energy Research Initiative (NERI) of the U.S. Department of Energy (DOE)
- ❑ The primary project objectives were to **develop the conceptual design for a safe and economic small, natural circulation light water reactor**
- ❑ Installed and operated at Oregon State University

| # | QUANTITY | Unit | Value |
|---|--|------|--------|
| 1 | Tot. No. of HYDR volumes | -- | 319 |
| 2 | Tot. No. of HYDR junctions | -- | 378 |
| 3 | Tot. No. of HYDR subvolumes in the core | -- | 6 |
| 4 | Tot. No. of heat structures | -- | 314 |
| 5 | Tot. No. of mesh points in the heat structures | -- | 3310 |
| 6 | Tot. No. of core active structures (radial x axial meshes) | | 17 x 6 |





MASLWR: validation activities

RELAP5-3D MASLWR blind calculations

□ Pretest calculation of two scenarios

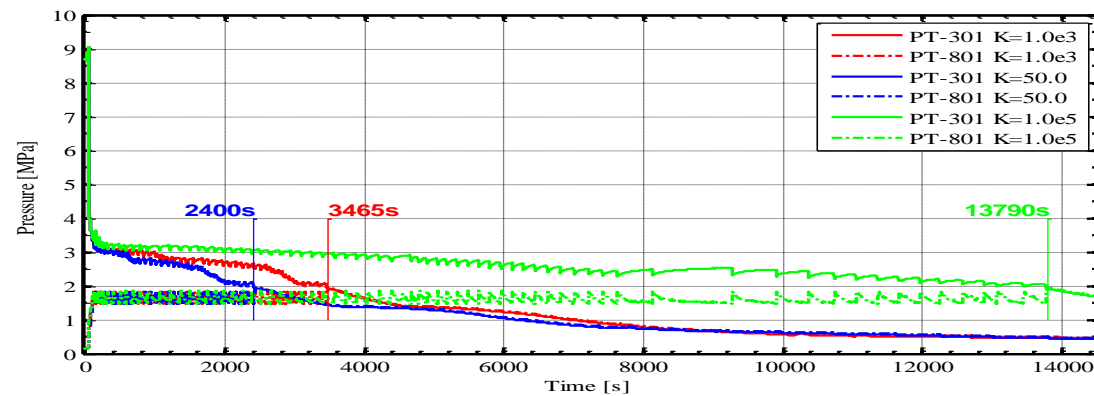
- *SP-2: Loss of Feedwater Transient with Subsequent ADS Operation and Long Term Cooling*
 - *Thermal stratification, natural convection, circulation and steam condensation in large pools of liquid*
 - *Single phase, two-phase and intermittent natural circulation*
- *SP-3: Normal Operating Conditions at Different Power Levels*
 - *Natural circulation*
 - *Heat transfer in helical tubes*



MASLWR: validation activities

RELAP5-3D SP-2 blind calculation

- ❑ Primary vessel and Containment vessel are modeled as two parallel vertical stacks of volumes
 - In order to simulate internal circulation and mixing;
 - Containment vessel parallel volumes are interconnected with cross-flow junctions
- ❑ Primary side depressurization time sensible on K-loss at the cross-jun in containment model
 - different mixing degree

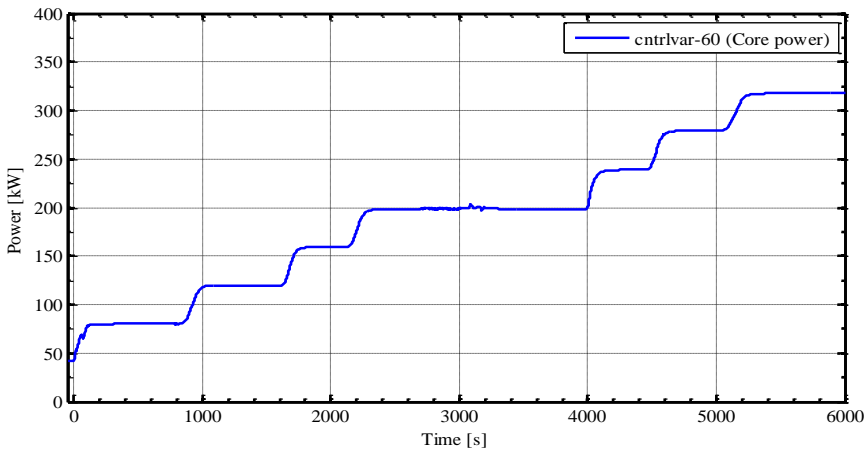




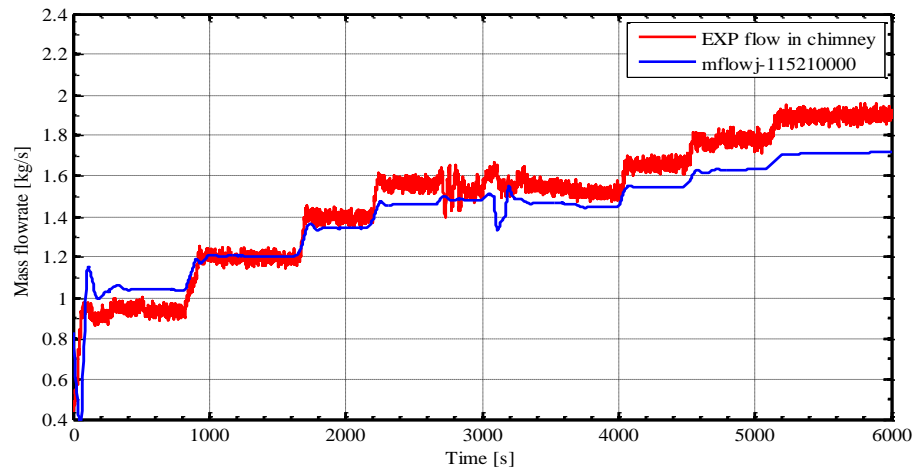
MASLWR: validation activities

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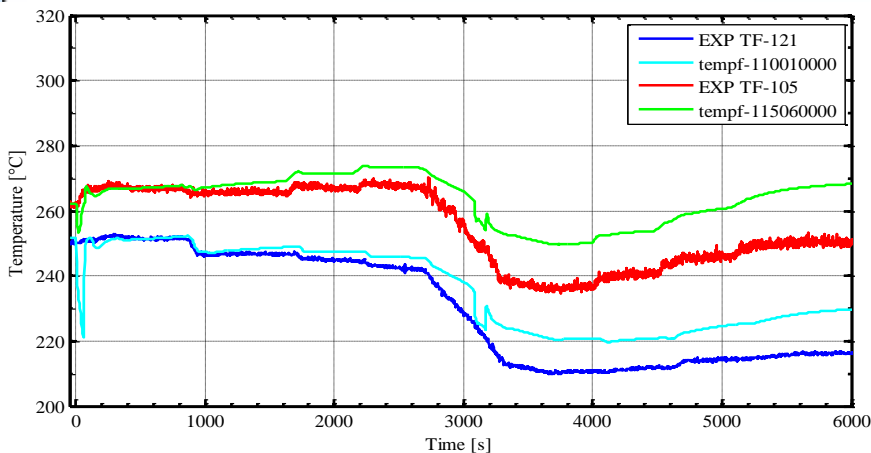
RELAP5-3D SP-3 blind calculation



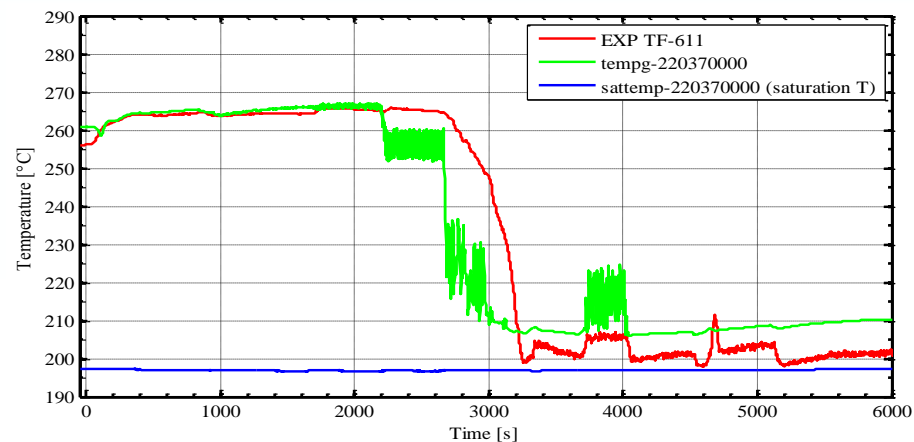
Core power



Primary side mass flow



Core inlet/outlet temperature



Sec.side steam outlet temperature



OECD benchmarks

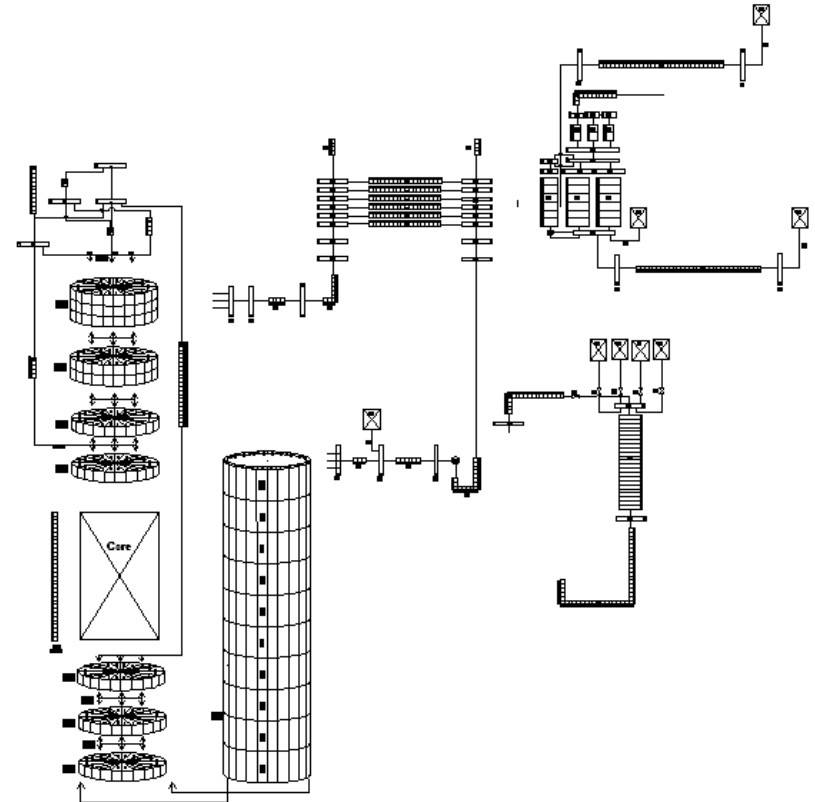
- ❑ GRNSPG is involved in many OECD projects

- ❑ Recent (on-going) activities with Relap5-3D
 - Oskarshamn benchmark
 - Kalinin 3 benchmark



Kalinin 3 BENCHMARK : MODELS

- ❑ VVER 1000 NPP
- ❑ RELAP5-3D TH model developed by GRNSPG
- ❑ RELAP5-3D/Point kinetics SS and transient calculation. **SUBMITTED**
- ❑ RELAP5-3D/NESTLE for 3D-NK model: Best estimate coupled code plant transient modeling. **ONGOING**



- Primary side and SGs



K-3 BENCHMARK: TH & 3D-NK modeling

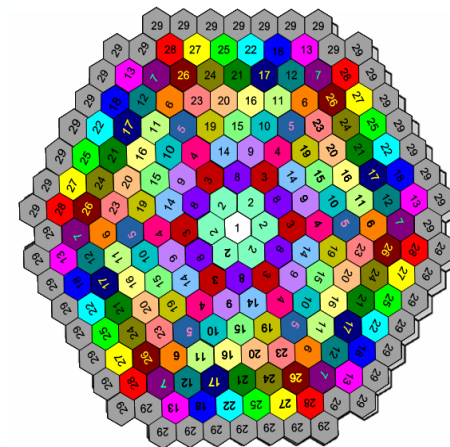
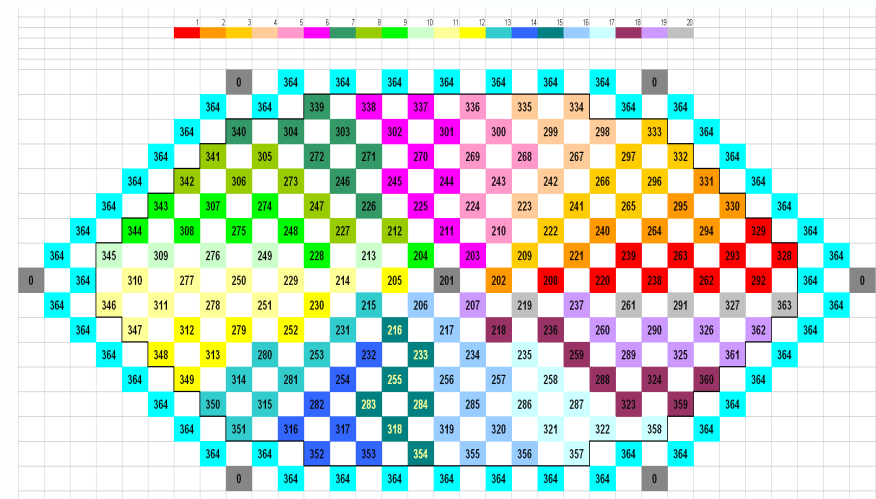
TH MODEL

- Particular care was devoted to the RPV modeling
 - 3D modeling of Downcomer (20 azimuthal sectors = 18 deg, 10 axial levels)
 - 3D Modeling of LP, UP, Lower and Upper Core Plate (always 20 azimuthal sectors)
 - 1D modeling for the UH
 - Radial, Upper and Bottom Reflector modeled
 - 32** axial layers (2 for top/bottom reflector, **30 for the core**)

3D-NK MODEL

- 6752 NK nodes
- Radial, Upper and Bottom Reflector modeled
- 32** axial layers (2 for top/bottom reflector, **30 for the core**)
- Up to 840 unrodded + **330** rodded compositions

FA versus azimuthal sectors (1-20)





K-3 BENCHMARK: Exercise 1 (MCP-1 trip)

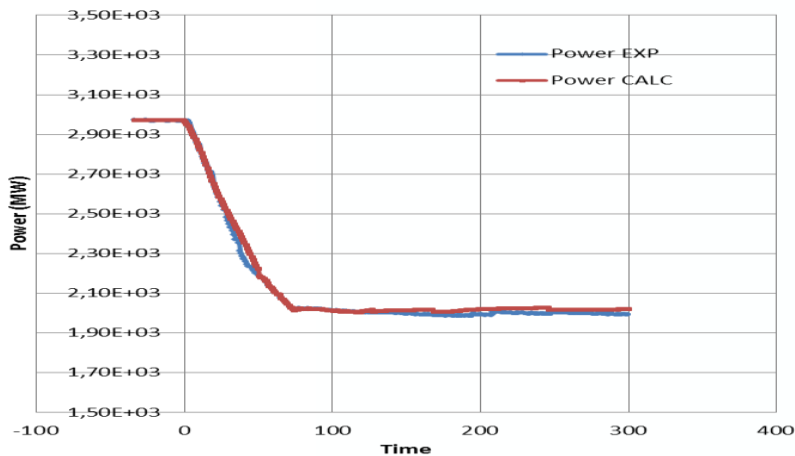
- Exercise 1 has been executed.
 - Steady state: Null-transient option for achieving SS
 - Checking main parameters for verifying consistency between experimental and calculation data
 - Transient: MCP-1 off, CR #10 & #9 moving, according to the Benchmark specifications

| Parameter | SS | | | Transient | | |
|--|------------|-------------|---------------|------------|-------------|---------------|
| | Experiment | Calculation | Deviation (%) | Experiment | Calculation | Deviation (%) |
| Power, MW | 2970.00 | 2970.00 | 0.00 | 1996.00 | 2017.00 | 1.05 |
| PRZ level,m | 8.60 | 8.69 | 1.03 | 7.99 | 7.82 | - |
| Average heating in the reactor core °C | 29.03 | 28.77 | 0.87 | 22.38 | 22.55 | 0.75 |
| SG #1 pressure, MPa | 6.26 | 6.29 | 0.47 | 6.02 | 5.98 | -0.66 |
| SG #2 pressure, MPa | 6.29 | 6.30 | 0.15 | 6.27 | 6.20 | -1.11 |
| SG #3 pressure, MPa | 6.25 | 6.28 | 0.48 | 6.23 | 6.22 | -0.16 |
| SG #4 pressure, MPa | 6.24 | 6.31 | 1.12 | 6.16 | 6.14 | -0.32 |
| Coolant flow rate in loop #1, kg/s | 4635.00 | 4635.00 | 0.00 | -1530.00 | -1883.00 | 23.07 |
| Coolant flow rate in loop #2, kg/s | 4639.00 | 4635.00 | -0.09 | 5145.00 | 5288.96 | 2.72 |
| Coolant flow rate in loop #3, kg/s | 4550.00 | 4552.00 | -0.04 | 5083.00 | 5120.80 | 0.72 |
| Coolant flow rate in loop #4, kg/s | 4550.00 | 4557.00 | 0.15 | 5200.00 | 5270.36 | 1.35 |
| Total coolant flow rate, kg/s | 18340.00 | 18379.00 | 0.21 | 13900.00 | 13794.10 | -0.08 |
| CL coolant temp in loop #1 | 288.00 | 287.90 | 0.03 | 284.90 | 284,48 | -0.14 |
| CL coolant temp in loop #2 | 287.80 | 288.00 | 0.07 | 287.40 | 287,18 | -0.08 |
| CL coolant temp in loop #3 | 287.60 | 289.80 | 0.76 | 288.00 | 289.84 | 0.66 |
| CL coolant temp in loop #4 | 287.50 | 287.90 | 0.14 | 284.90 | 283,85 | -0.36 |
| HL coolant temp in loop #1 | 317.40 | 316.70 | -0.22 | 276.90 | 273.17 | -1.36 |
| HL coolant temp in loop #2 | 317.40 | 317.00 | -0.13 | 311.70 | 311.77 | 0.02 |
| HL coolant temp in loop #3 | 316.40 | 318.20 | 0.57 | 313.60 | 315.90 | 0.73 |
| HL coolant temp in loop #4 | 317.20 | 316.80 | -0.13 | 304.01 | 300.94 | -1.00 |

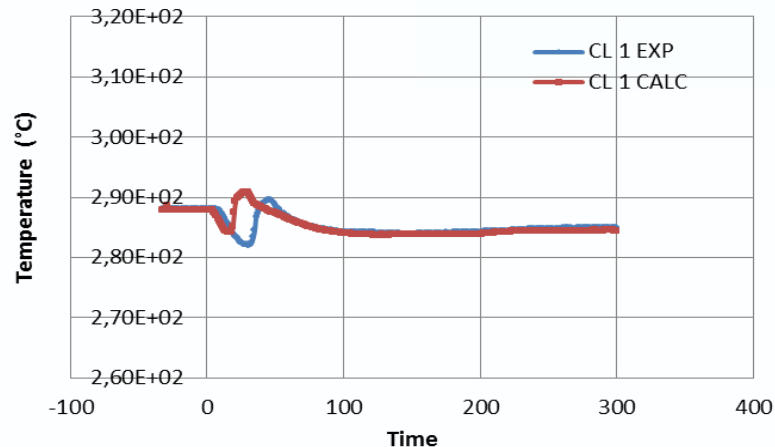


K-3 BENCHMARK: Selected results

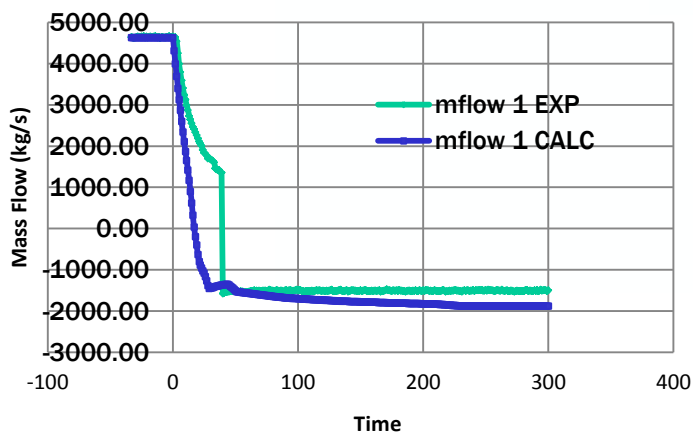
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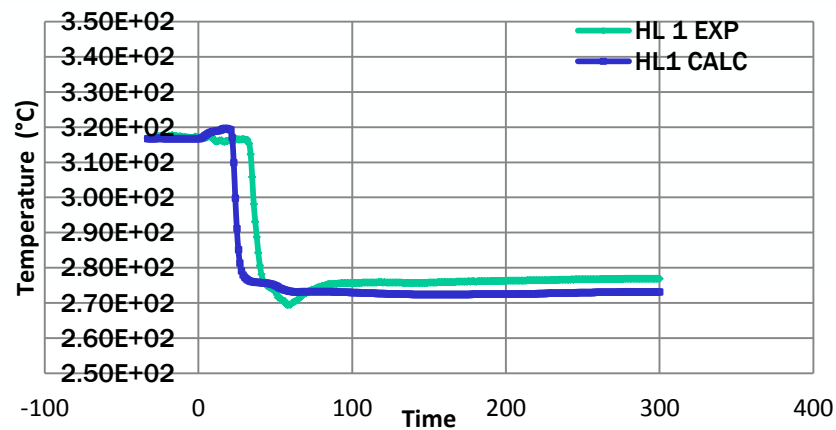
Power



CL coolant temperature Loop #1



Coolant Flow Rate Loop #1



HL coolant temperature Loop #1



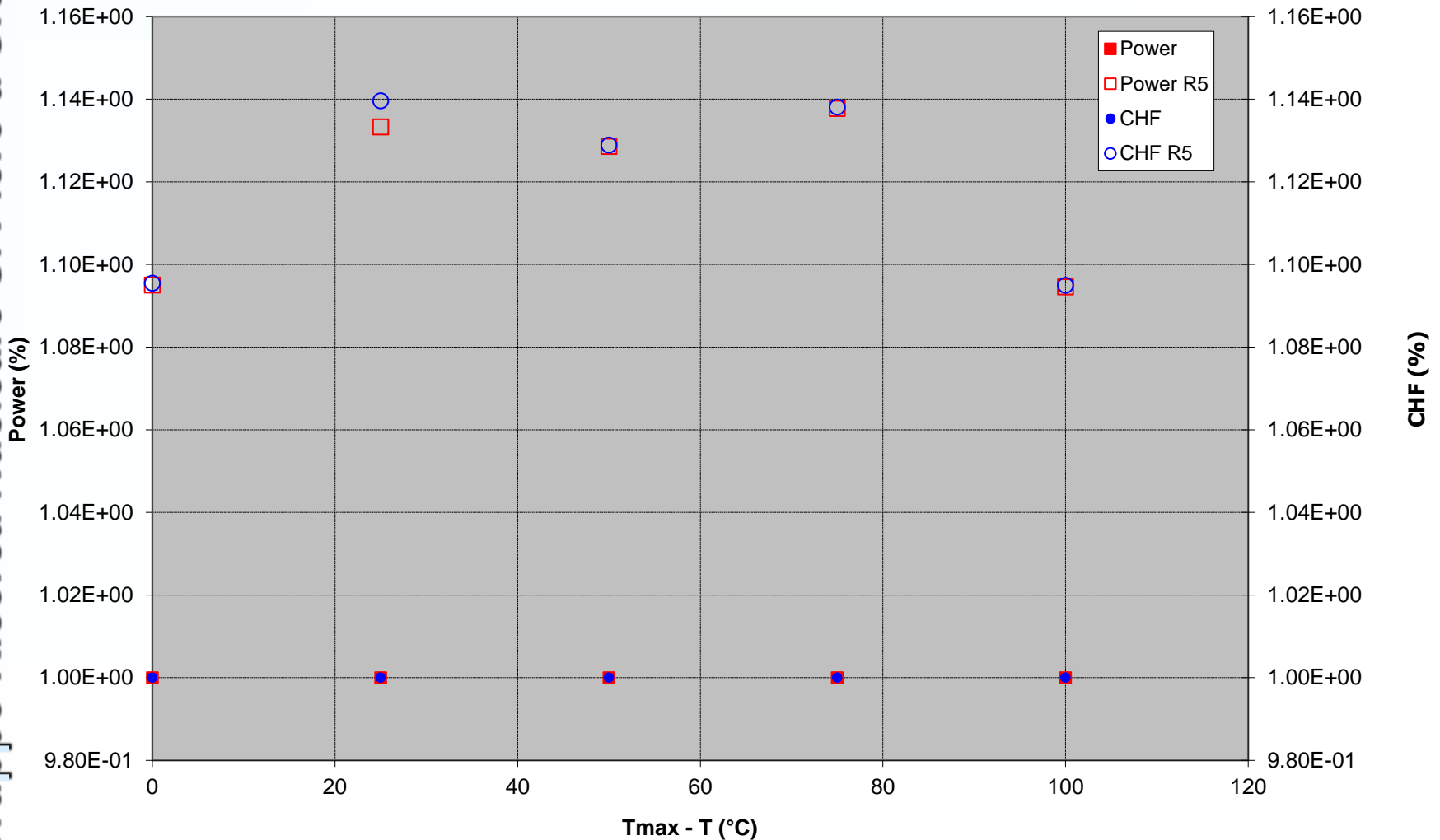
CHF in low mass flux condition

- ❑ Pre-test activity
- ❑ Support to the design of an experimental facility (flat profile)
- ❑ Benchmark between Relap5-3D 2.4.2 and COBRA-EN (EPRI corr.)
- ❑ 30 calculations performed
 - Different pressure, mass flux, inlet temperature
- ❑ Discrepancy on CHF prediction: 10% to 30%
- ❑ Future activities:
 - 100 calculations
 - Use of Relap5-3D 4.0.3 (due to fixies in Groenevald look up tables)



CHF in low mass flux condition

□ Power and CHF discrepancy between Relap5-3D and COBRA-EN (1 case)





Turbulence in Relap5-3D

- Relap5-3D 4.0.3: capability to describe turbulent effect in MULTID components (option 31)
- Boron dilution test in ROCOM facility
- Main scopes of the (future) activity:
 - Comparison with TRACE and CATHARE codes capability in describing mixing phenomena
 - Comparison with experimental data
 - Accuracy evaluation by FFTBM
 - Paper submitted to NURETH 15



CONCLUSION

- ❑ GRNSPG activities related with Relap5-3D applications presented
- ❑ Activities attain to applied (FSAR) and validation (benchmarking) research
- ❑ Activities conducted following developed methodologies (e.g. SCRAD)
- ❑ Internal code validation benefits of:
 - Availability of huge experimental databases
 - Participation to international projects

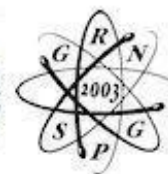


Thank you

... and don't miss

May 12-17, 2013 Pisa (Italy)

NURETH-15



15th International Topical Meeting on Nuclear Reactor Thermalhydraulics