



Idaho National Laboratory

# Evolving the ATHENA Model of a LOCA Analysis for the Generation IV Gas-cooled Fast Reactor

**Ryan Winningham**

The Ohio State University

August 15, 2005

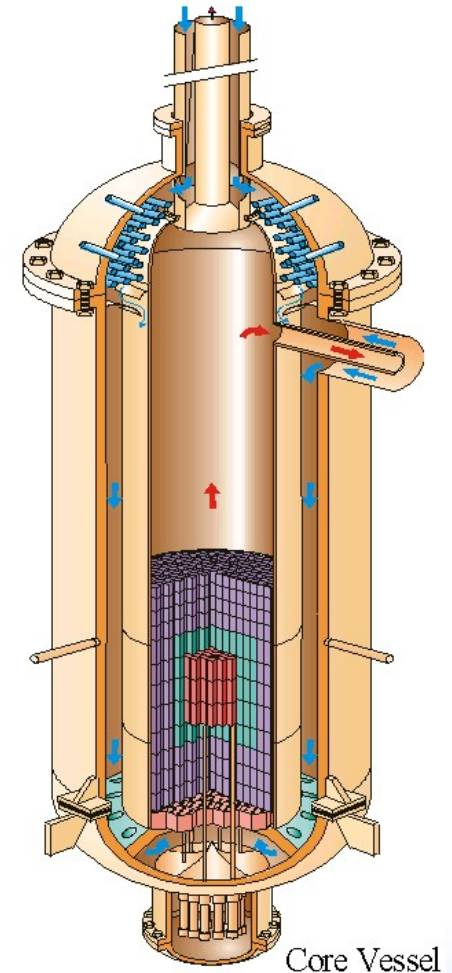
Mentor: Theron Marshall Ph.D.

# Presentation Outline

- **Overview of RELAP5/ATHENA GFR model**
- **Outline of Research Tasks**
- **Completed Work**
- **Work in Progress**
- **Future Work**
- **Questions**

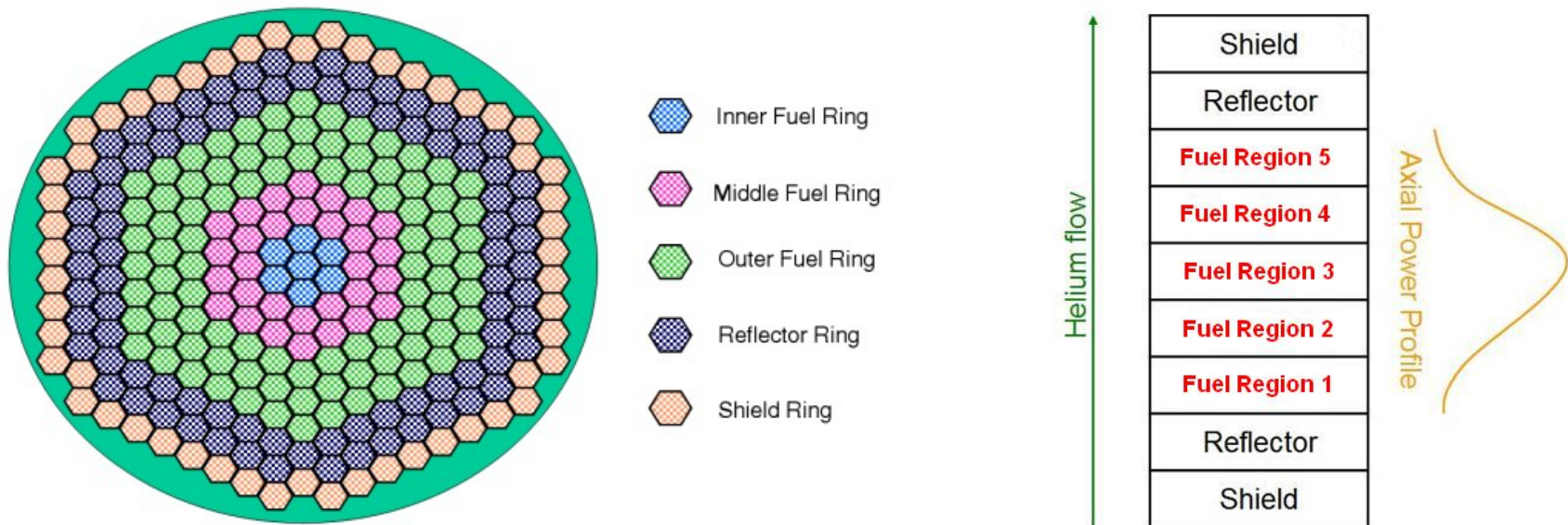
# Generation IV Helium Gas-Cooled Fast Reactor

- The Gas-Cooled Fast Reactor (GFR) is one of six Generation IV designs
- The 600MW<sub>th</sub> GFR uses a direct-cycle helium turbine for electricity generation, or can optionally use its process heat for thermochemical production of hydrogen due to the 850°C outlet temperature
- Through the combination of a fast spectrum and full recycle of actinides, the GFR minimizes the production of long-lived radioactive waste.



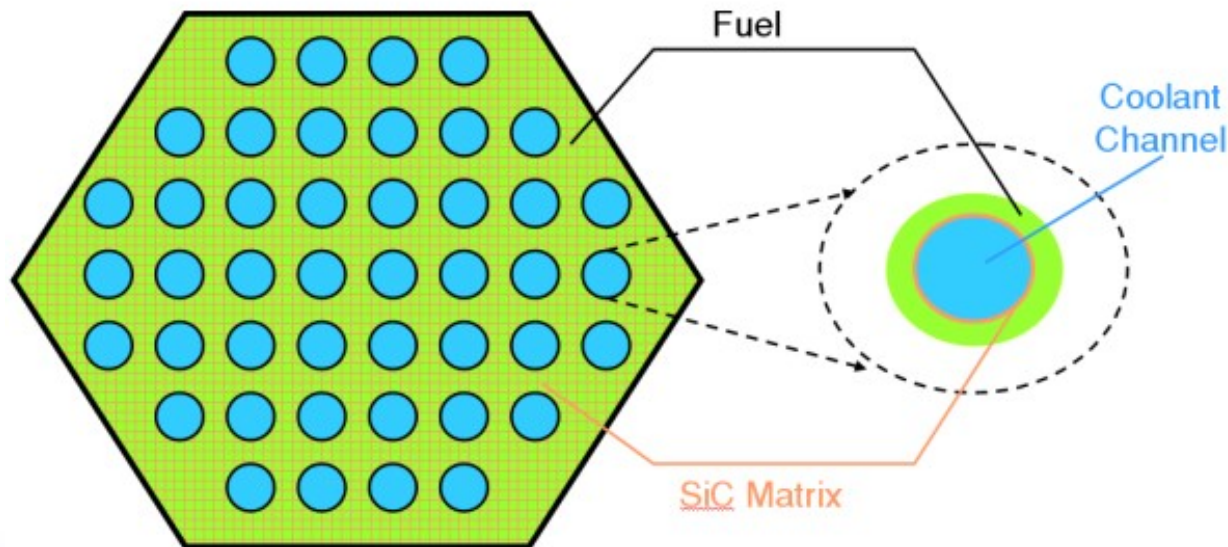
# RELAP5/ATHENA GFR Core Layout

- Three radial core sections (Inner Ring, Middle Ring, Outer Ring)
- Five axial core regions per ring

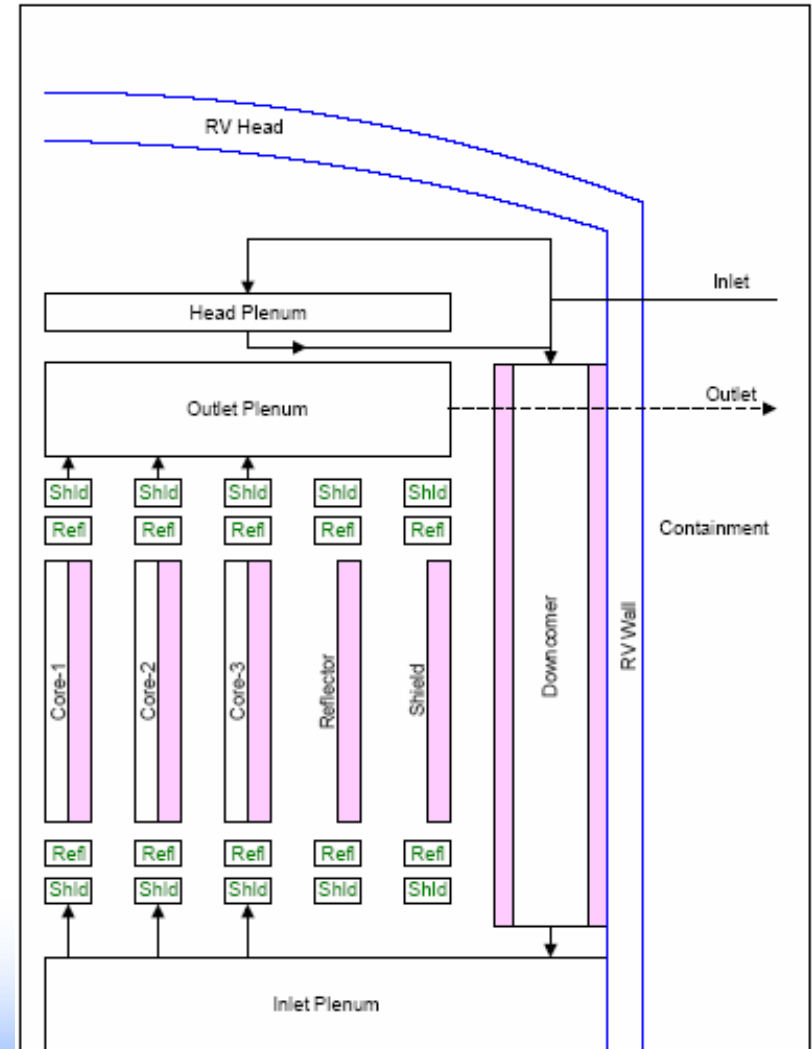
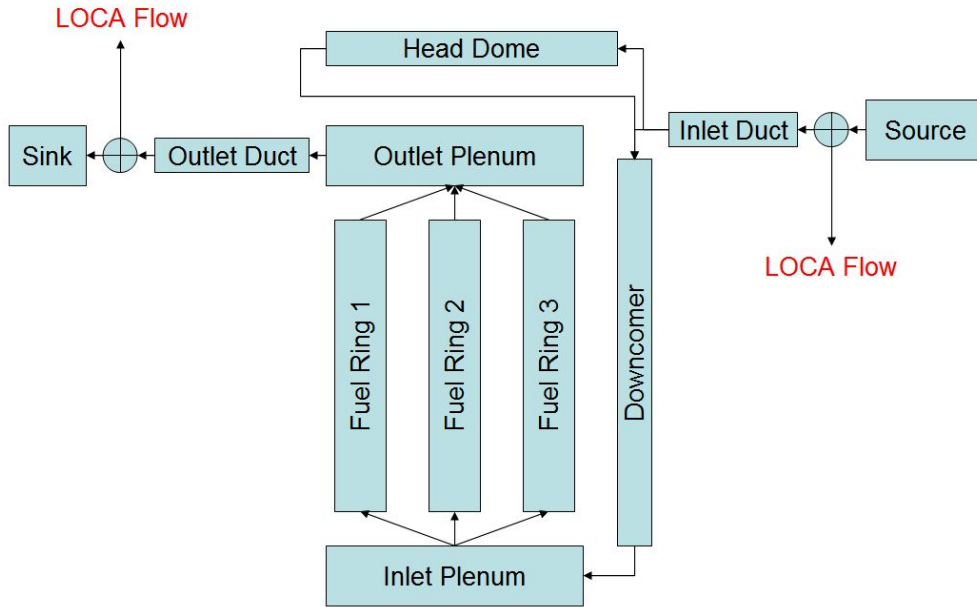


# Fuel Design

- The GFR prismatic fuel block contains fuel material dispersed in a SiC matrix
- Same unit cell methodology that is used in VHTR thermal analysis



# Hydrodynamic Volumes and Heat Structures



# Outline of Research Tasks

**Task 1 - Development of a hot channel**

**Task 2 - Radial and axial flux distribution**

**Task 3 - Inlet plenum orificing**

**Task 4 - SiC thermal conductivity investigation**

**Task 5 - LOCA transient / Containment modeling**

**Task 6 - GFR core modeling in FLUENT**

# Development of a Hot Channel

- **Two tasks for different needs**
  - **Hot channel as a heat structure (fuel temperature monitoring)**
  - **Hot channel as a hydrodynamic volume and heat structure (coolant property monitoring – used for stability analysis, FLUENT comparison)**

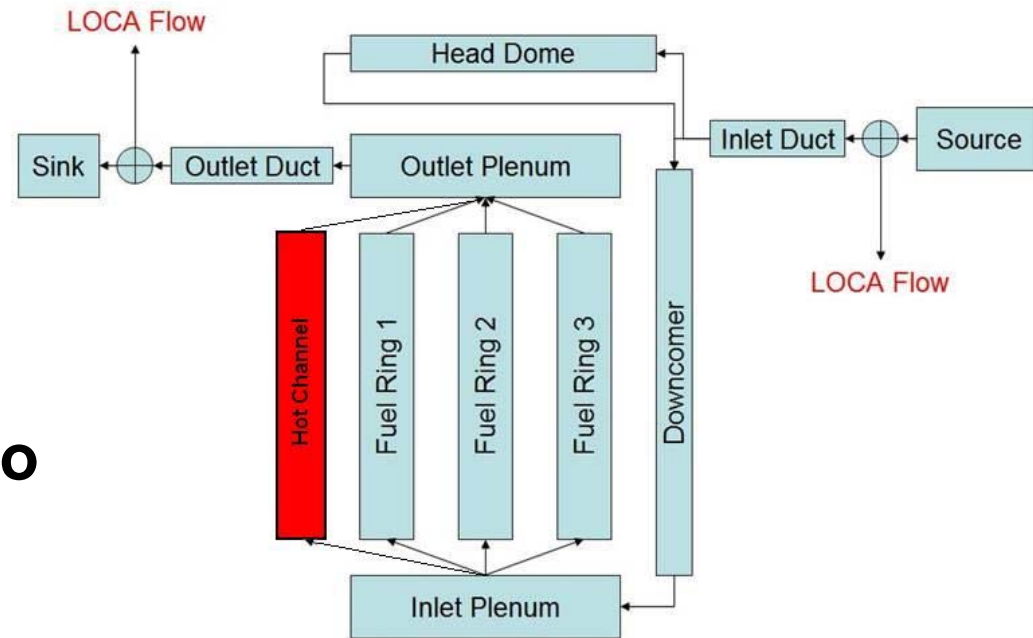


# Hot Channel as a Heat Structure

- **Hot channel heat structure added to inner core ring**
- **The heat structure represents the equivalent annulus of fuel for one coolant channel**
- **There are 637 coolant channels in the inner core ring (7 assemblies, 91 coolant channels each)**
- **No impact on inner ring coolant temperatures**

# Hot channel as a Hydrodynamic Volume and Heat Structure

- New hydrodynamic volume added to core geometry to represent a single coolant channel
  - Removed one channel from inner ring
- Heat structure added to the single hot channel
- Provides fuel and coolant property data for the hot channel

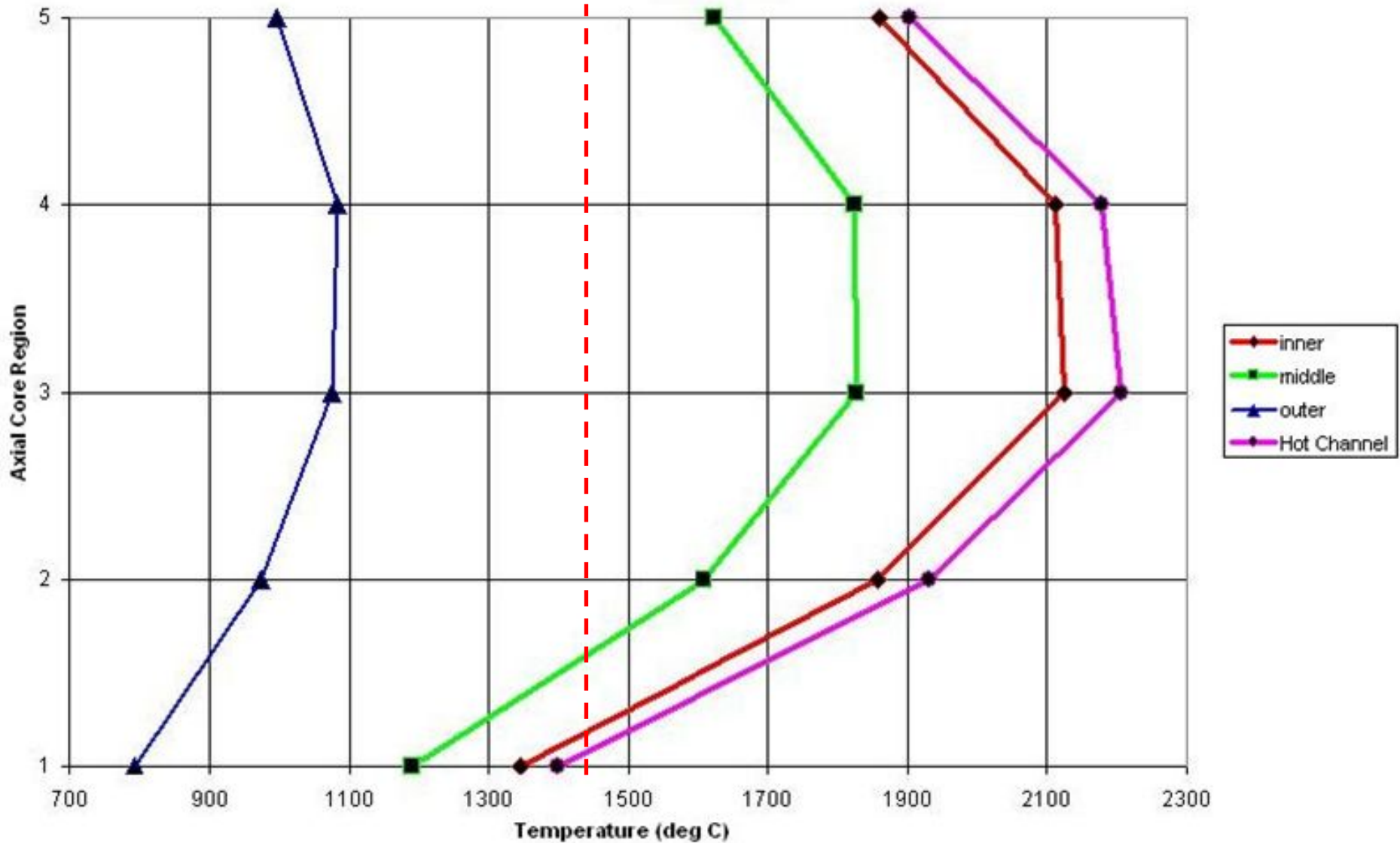


# Radial and Axial Flux Distribution

- **5 Axial increments**
  - **1.25 peak-ave power ratio (chopped cosine)**
- **3 (+1 Hot Channel) Radial increments**
  - **1.5 peak-ave power ratio (chopped cosine)**
    - **1.5 peak is placed in the hot channel**

# Results of Core Power Distribution

Axial Temperature Distributions



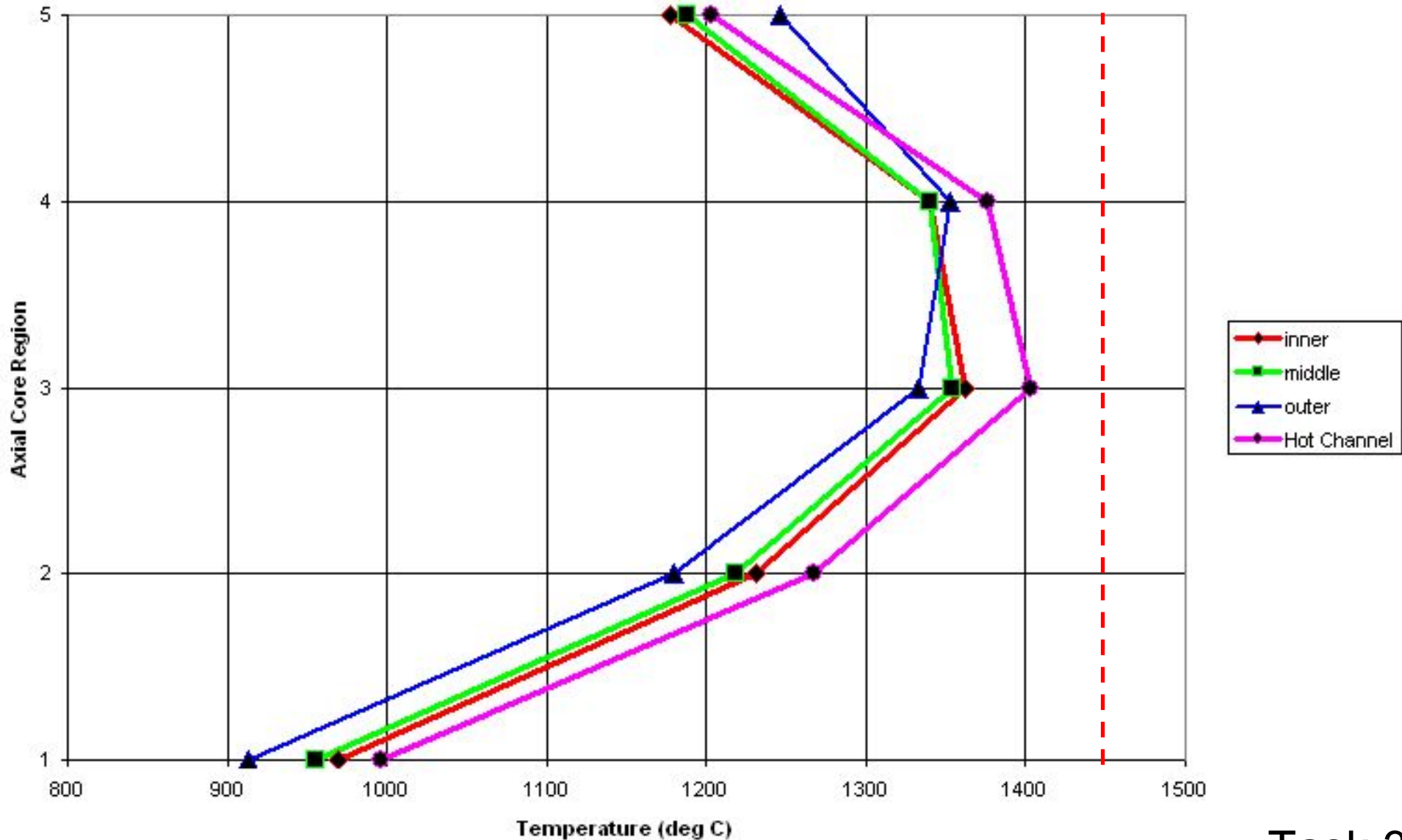
# Inlet Plenum Orificing

- Inlet plenum orificing is necessary in order to meet GFR maximum fuel temperature design specifications
  - 1450 °C normal operation
  - 1650 °C transient

	% Constriction	Flow area (m <sup>2</sup> )	Mass Flow rate (kg/sec)	% of total flow
Inner Ring (7)	<b>0.0%</b>	<b>0.1456</b>	<b>43.04</b>	<b>13.2%</b>
Middle Ring (30)	<b>52.0%</b>	<b>0.2996</b>	<b>140.4</b>	<b>43.3%</b>
Outer Ring (90)	<b>85.5%</b>	<b>0.2714</b>	<b>141.9</b>	<b>43.6%</b>

# Results of Inlet Plenum Orificing

## Axial Temperature Distributions

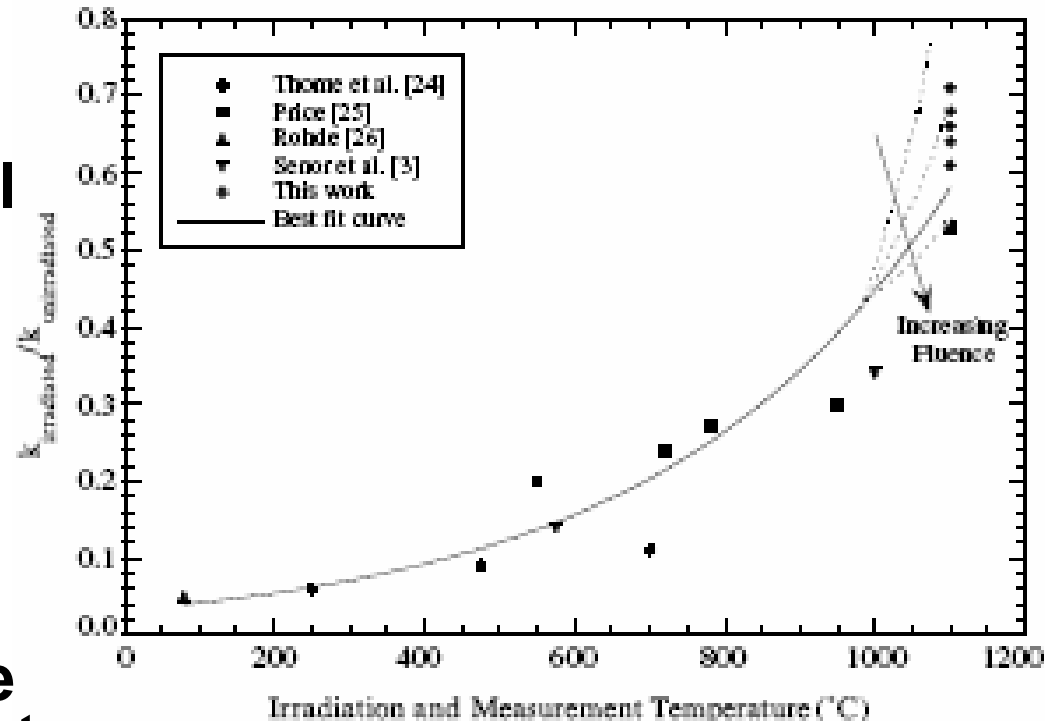


# Impacts of Inlet Plenum Orificing

- Increase in core pressure drop from 14 kPa to 73 kPa
- Increased pumping power from 1.0 MW to 5.5 MW (0.9% thermal power)
- Orificing optimized for end of life core fuel temperatures (high peaking)
  - adjustable bypass flow or fresh fuel flux shaping necessary at beginning of life core

# SiC Thermal Conductivity Investigation

- SiC thermal conductivity drops by  $1/2$  -  $1/3$  with radiation exposure
- The change in thermal conductivity can increase fuel temperatures by as much as  $150\text{ }^{\circ}\text{C}$  (conductivity lowered by  $1/3$ )
- With GFR fast flux  $\sim 10^{15}$  n/cm<sup>2</sup>-sec, these effects may be seen just weeks from startup



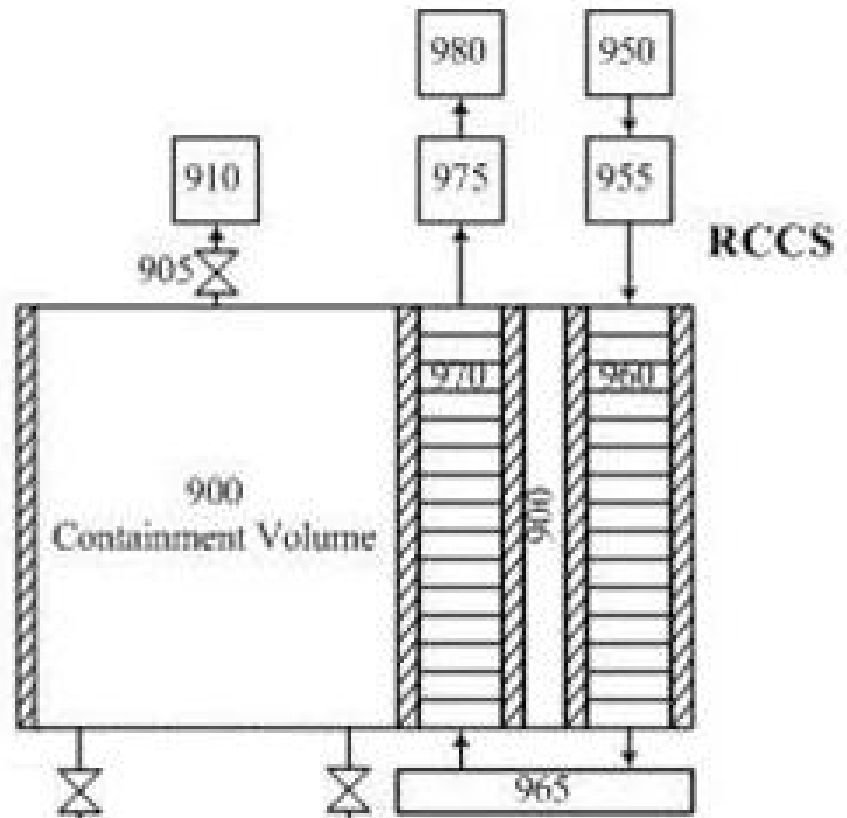
*D.J. Senor et al. / Journal of Nuclear Materials 317 (2003) 145–159*





# RELAP5/ATHENA RCCS Model

- This is the same RELAP5/ATHENA model of the RCCS that is used in the VHTR
- Air at 27°C enters the inlet plenum (955)
- Then flows down the downcomer (960) attached to the containment wall
- Then up the riser channels (970) and discharged to the upper plenum (975)



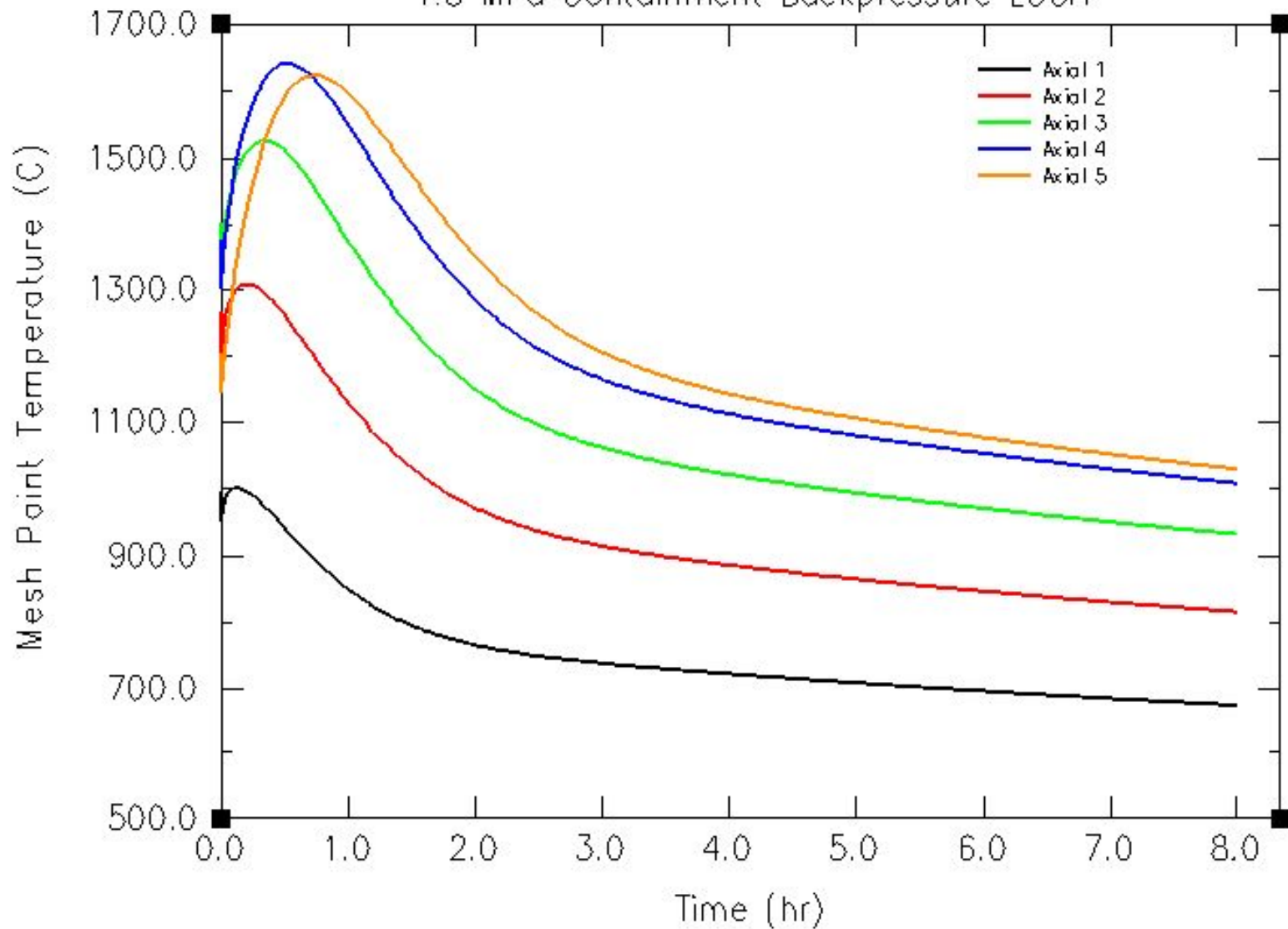
# Containment Backpressure

- **The heat removal capacity of the RCCS is dependent on the containment pressure (air density)**
- **1.2 MPa Containment pressure was sufficient to passively cool the core and prevent fuel failure before the addition of the hot channel and radial-axial power distributions**
- **1.8 MPa is now necessary to meet GFR maximum fuel temperature design specifications (1650 °C transient)**

# RCCS Performance (Old Containment)

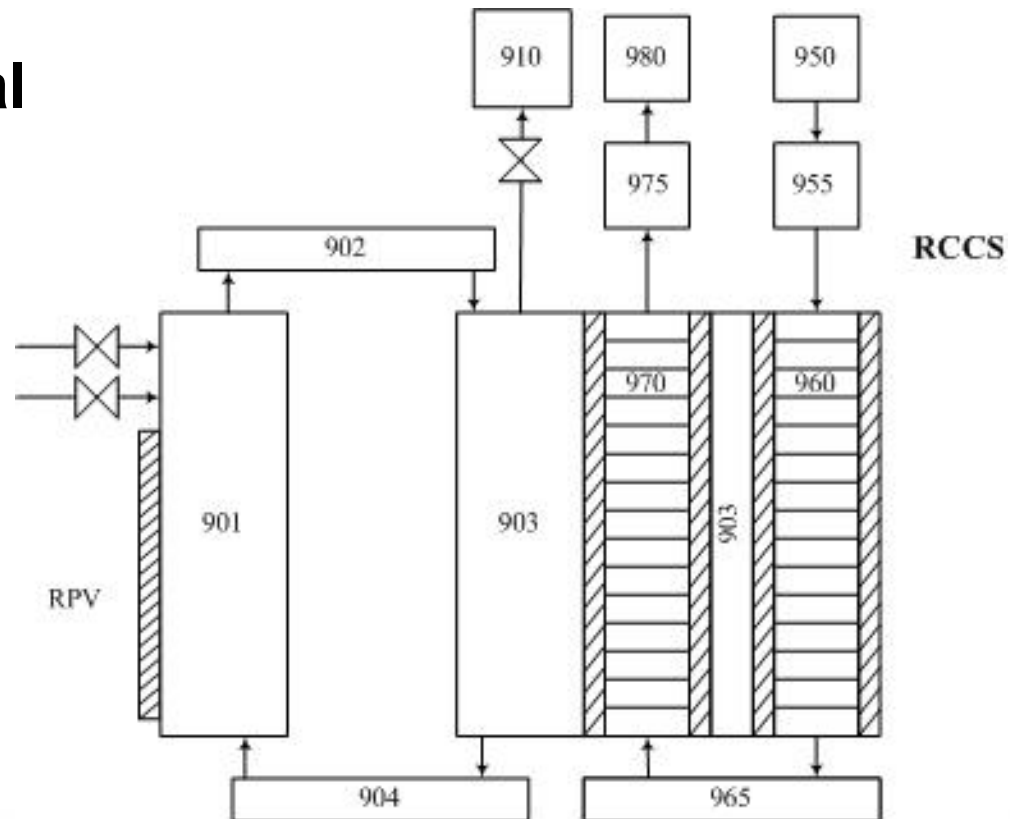
Hot Channel Fuel Temperatures

1.8 MPa Containment Backpressure LOCA



# New Containment Model

- Used to investigate heat removal by natural circulation in containment
- Containment modeled as two concentric annuli
- Loop flowrates will be based off FLUENT modeling results



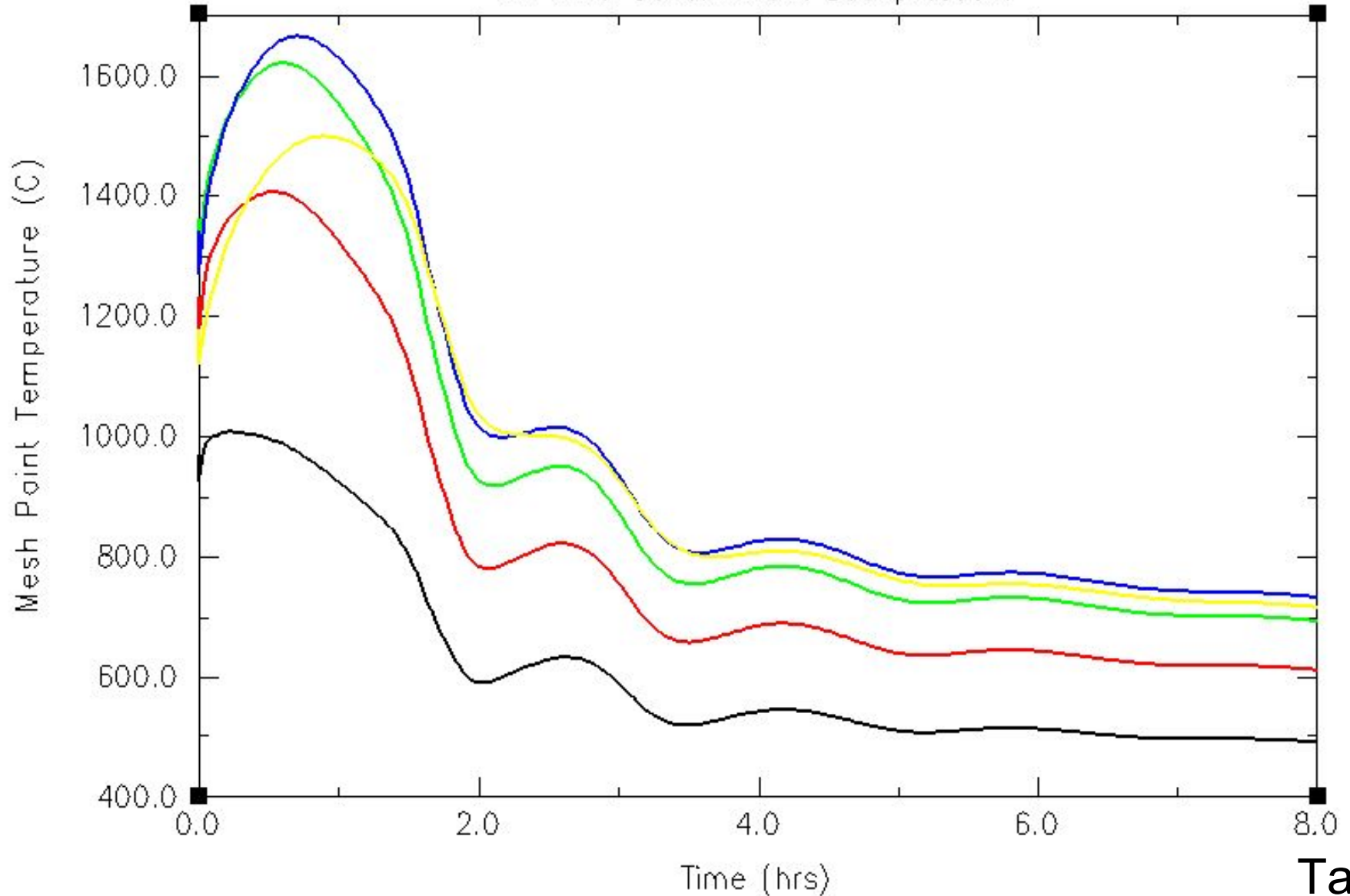
# **New Containment Model (Preliminary Results)**

- **Possible to lower containment pressure from 1.8MPa to 1.4MPa and still achieve 1650 °C transient depressurization design parameter**
- **Shows natural circulation in containment and the core**
- **Future Work**
  - **FLUENT benchmark of containment**
  - **Adjustment of containment size**
  - **Investigate flow instabilities**

# RCCS Performance (Preliminary Results)

Hot Channel Fuel Temperatures (New Containment)

1.4 MPa Containment Backpressure



# GFR Core Modeling in FLUENT

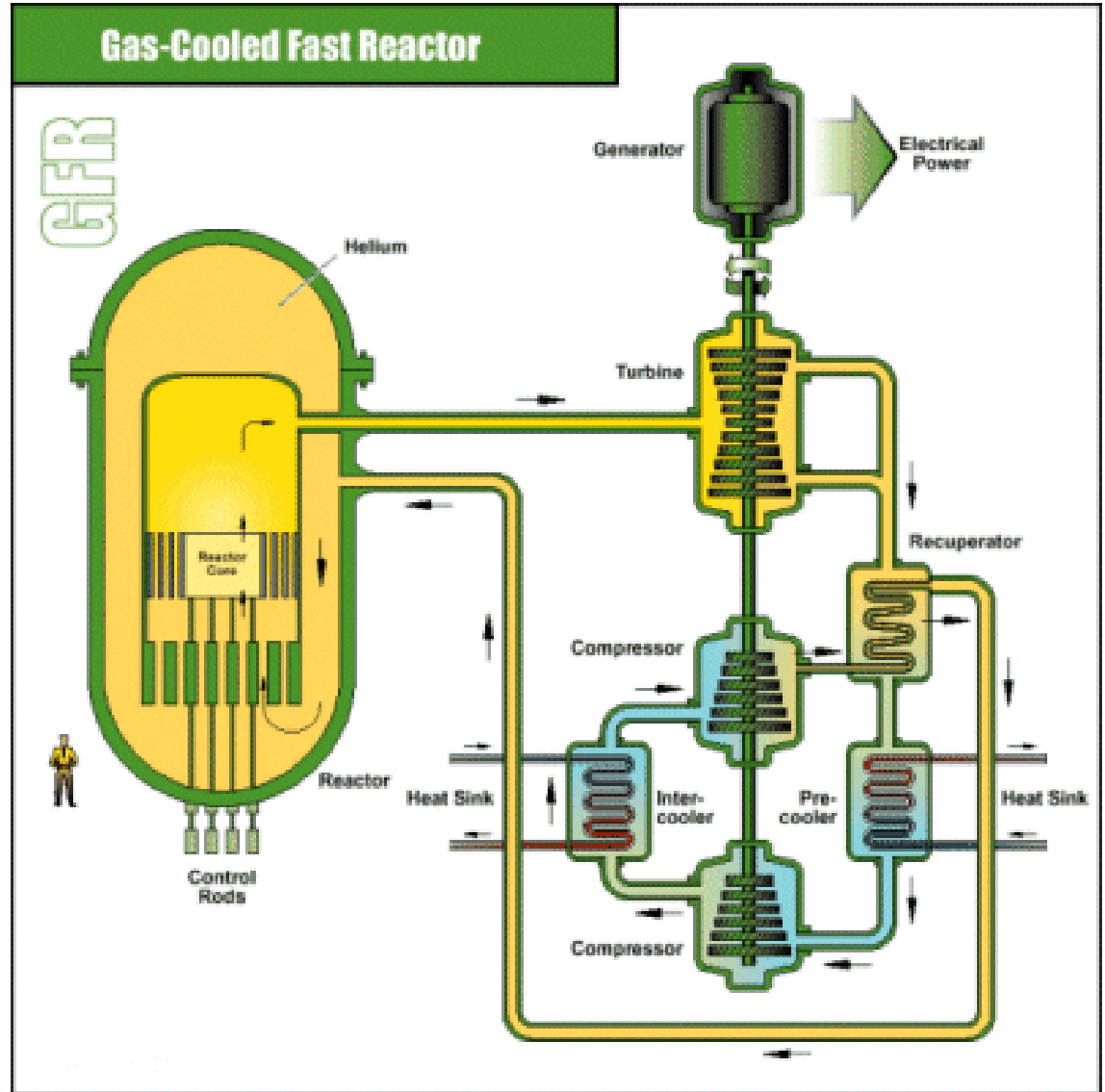
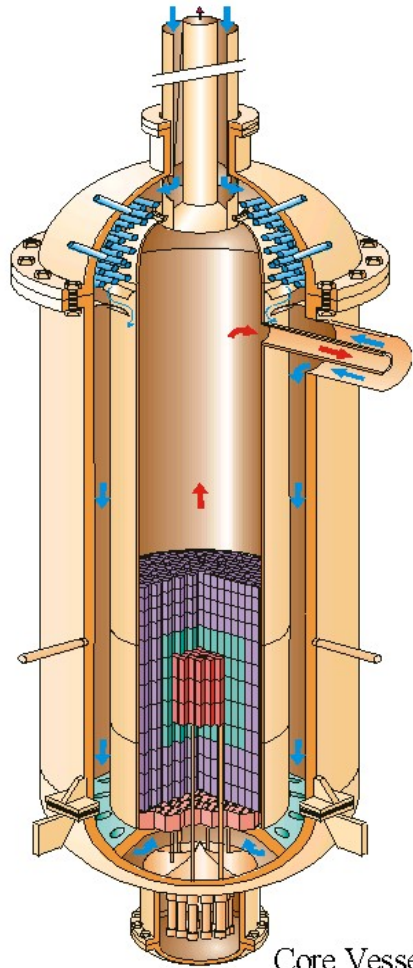
- **Created 3 FLUENT geometries to investigate core flow under natural circulation conditions.**
  - **Single coolant channel**
  - **3 channels with lower plenum (inlet)**
  - **3 channels with lower and upper plenum**
- **Benchmarked geometries against RELAP5/ATHENA GFR hydrodynamic hot channel**
- **Currently working on natural circulation flow and viscosity induced flow starvation.**



# Future Work

- **FLUENT modeling of Containment/RCCS decay heat removal for LOCA**
- **Update core design to align with the U.S./French I-NERI GFR concept (2400MW<sub>th</sub>)**

# Questions?



# References

- Theron Marshall, Kevan Weaver, and Cliff Davis, “IMPLICATIONS OF PASSIVE DECAY HEAT REMOVAL DURING A LOCA WITH A GAS-COOLED FAST REACTOR”, Proceedings of ICAPP '05, Seoul, KOREA, May, 2005
- D.J. Senior , G.E. Youngblood, L.R. Greenwood, D.V. Archer, D.L. Alexander, M.C. Chen, G.A. Newsome, “Defect structure and evolution in silicon carbide irradiated to 1 dpa-SiC at 1100 C”, Journal of Nuclear Materials 317 (2003) 145–159
- R. J. PRICE, “THERMAL CONDUCTIVITY OF NEUTRON-IRRADIATED PYROLYTIC  $\beta$ -SILICON CARBIDE”, Journal of Nuclear Materials 46 (1973) 268-272

# Acknowledgements

Larry Zirker, Kevan Weaver, Theron Marshall (INL)

Richard Christensen, Audeen Fentiman, Brian Hajek (OSU)

# Supplemental Slides

# Design Specs

Reactor Design Parameter	Conceptual Data
Power plant	600 MW <sub>th</sub>
Net efficiency	48% (helium, direct cycle)
Coolant pressure	9 MPa
Outlet coolant temperature	850°C (helium, direct cycle)
Inlet coolant temperature	490°C (helium, direct cycle)
Nominal flow and velocity	330 kg/s and 40 m/s
Core volume	10.9 m <sup>3</sup> (H/D ~1.7/2.9 m)
Core pressure drop	~ 0.04 MPa
Volume fraction (%) Fuel/Gas/SiC	50/40/10
Average power density	55 MW/m <sup>3</sup>
Reference fuel compound	(U, Pu)C/SiC (50/50%) 17% Pu
Breeding/Burning performances	Self-Breeder
Maximum fuel temperature	1174°C (normal operation) < 1650°C (depressurization)
Fuel management	multi-recycling
Primary vessel diameter	< 7 m